

103rd Annual T.H.E. Conference
February 28 & March 1, 2017
University of Illinois at Urbana-Champaign

Planning and Design
of
IL-104 BRIDGE
OVER
ILLINOIS RIVER

MEREDOSIA, IL

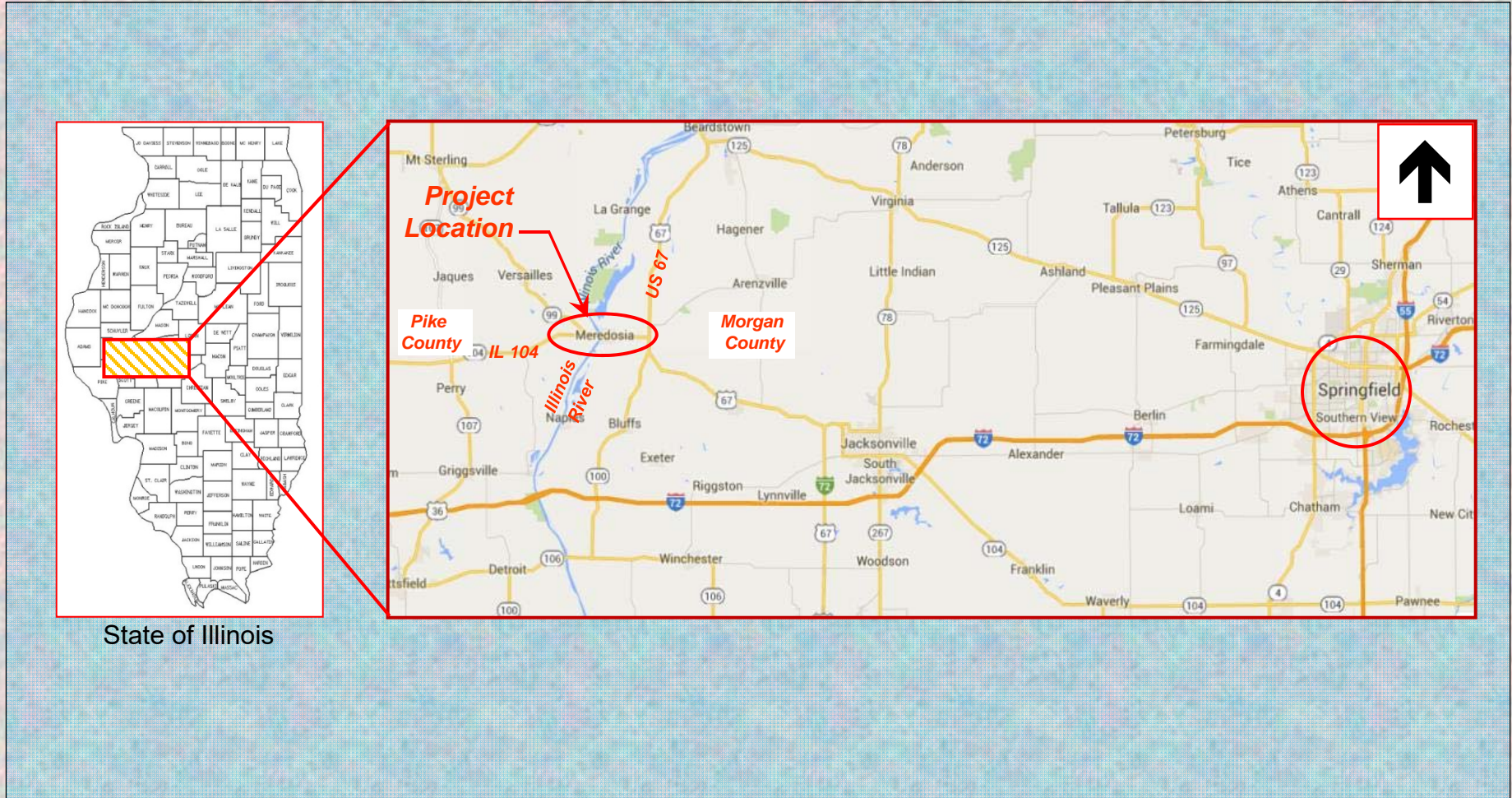
Presenter:
Vinod C. Patel, PE, SE
Exp US Services Inc.

Presentation Outline

1. **Project Overview**
2. Phase I Study (Preliminary Engineering)
3. Bridge Type Study
4. Bridge Design
5. Innovative Details
6. Analysis - Design
7. Construction



Project Location



State of Illinois



Why the project is needed?

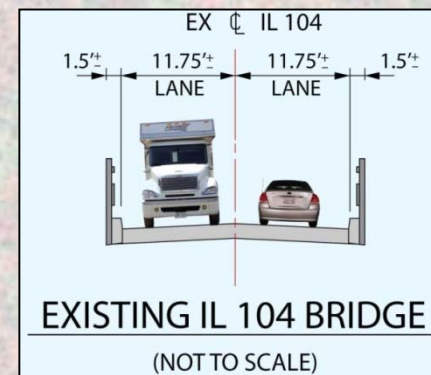
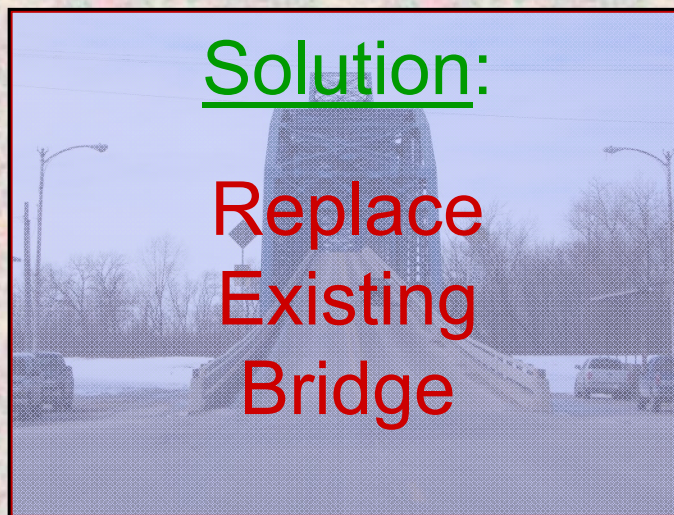
Existing Bridge:

- **Structurally Deficient** – Built in 1936 / 80 years old
Has deteriorated with age

Sufficiency Rating < 15 (out of 100)

Low Rating => Numerous elements with advanced deterioration;
Requires close monitoring & frequent maintenance / repairs

- **Functionally Obsolete** – Narrow Lanes / No Shoulders / Unsafe

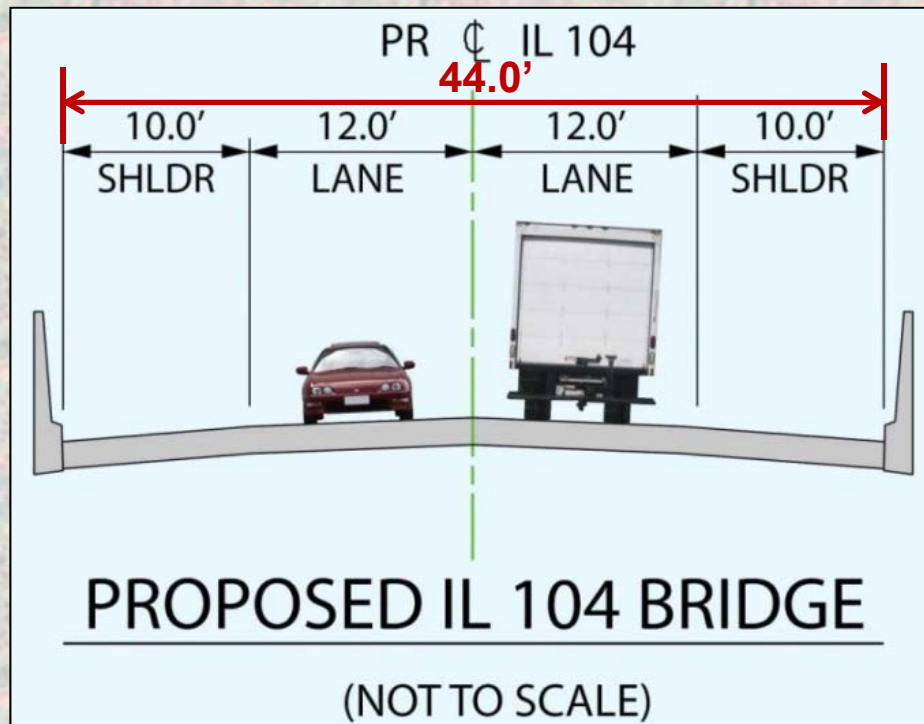


Presentation Outline

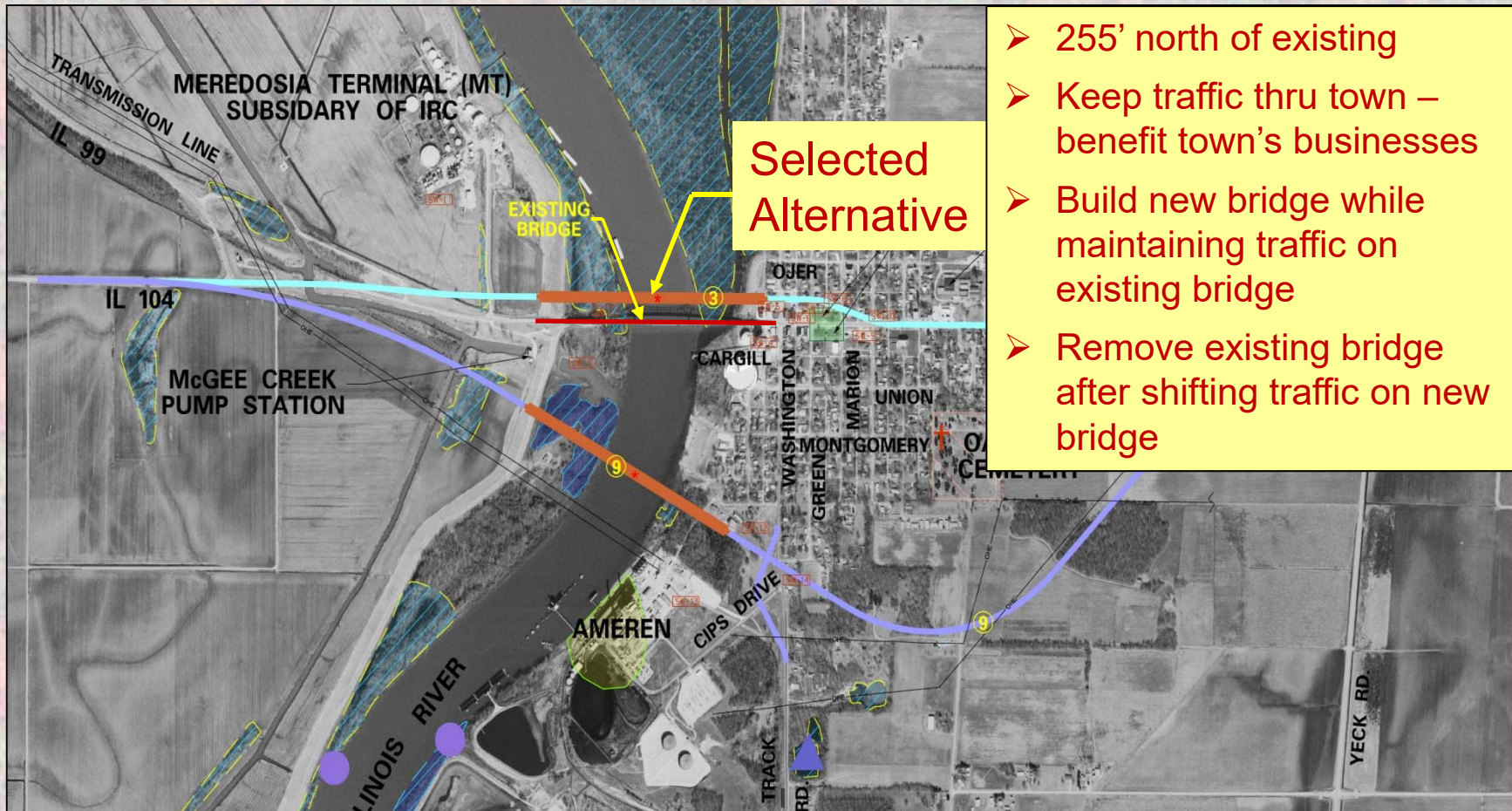
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New Bridge - What size to build?

Based on traffic volume, current design standards and the functional requirements -



Where to build?



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Bridge Type Study – Bridge Profile

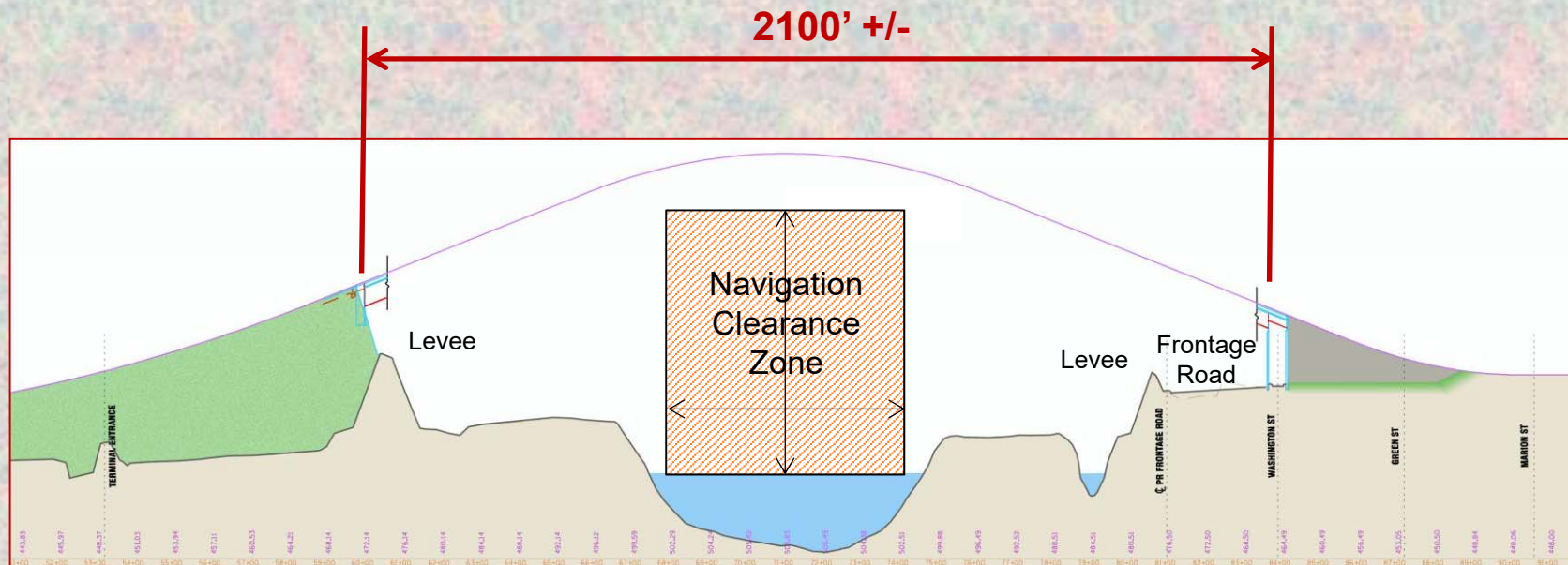
Illinois River → **A Navigational Waterway**

U.S. Coast Guard's Navigational Clearance Requirements:

Horizontal Clearance = **555 ft.**

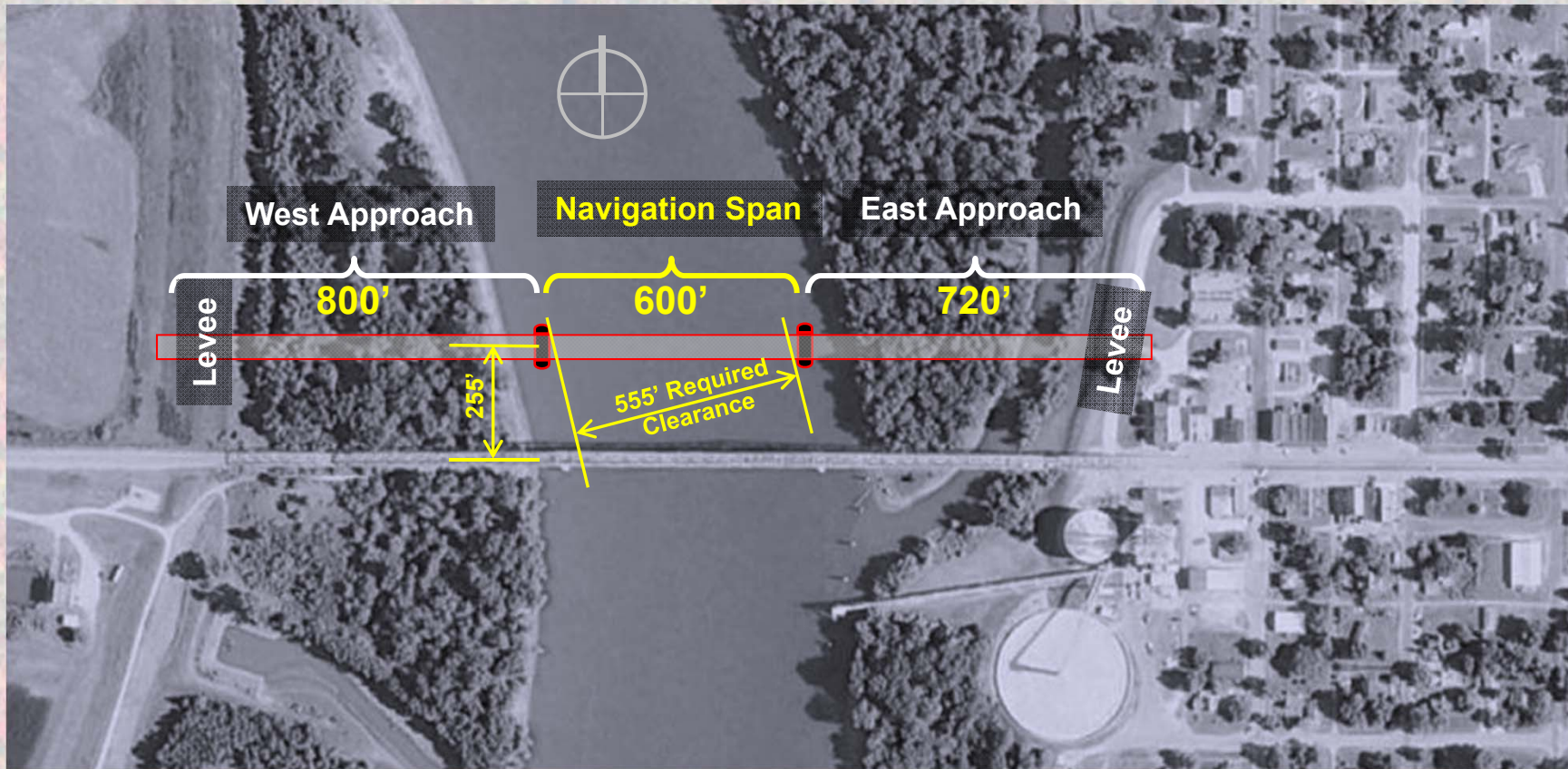
Vertical Clearance = **55 ft. above 2% Flowline**

Profile Grade = **4% Max.**



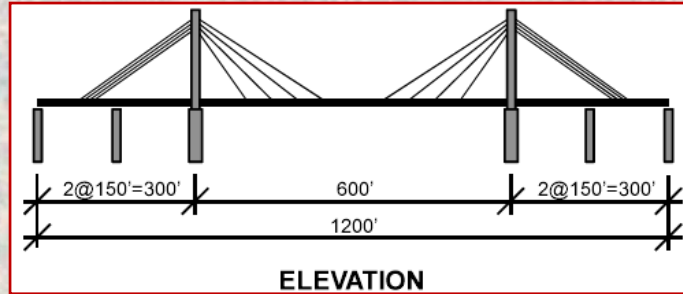
Bridge Type Study: Bridge Limits & Layout

Focus – Main Navigation Span

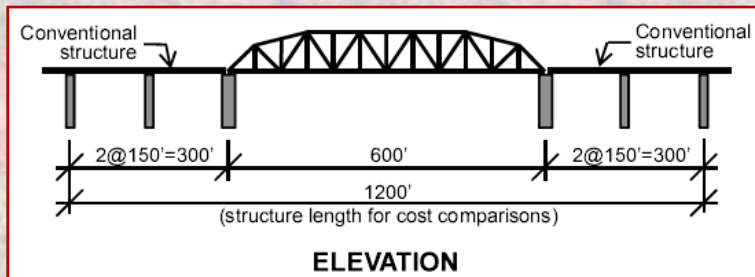


Bridge Type Study: Focus – 600' Main Navigation Span

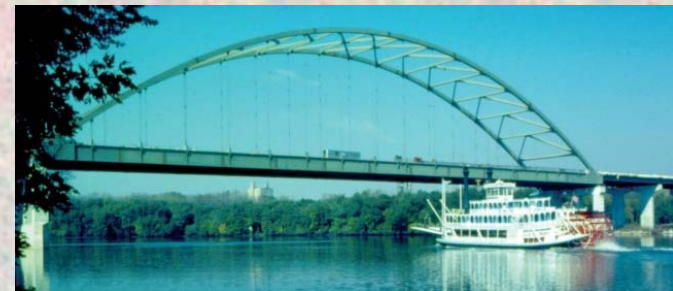
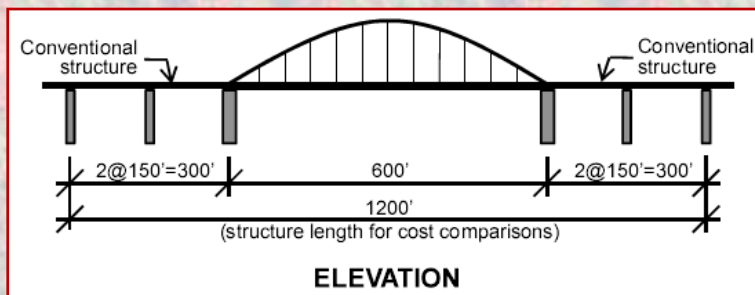
Cable-stayed



Truss



Tied-arch



Bridge Type Study

Evaluation Criteria → Evaluation:

- ❖ Costs – Initial & Life Cycle → virtually same for all
- ❖ Constructability → advantage Cable-stayed
- ❖ Inspection and Maintenance → advantage Arch
- ❖ IDOT Experience / Familiarity → advantage Arch

Selected Bridge Type → Tied-Arch

Selected Bridge Type → Tied-arch

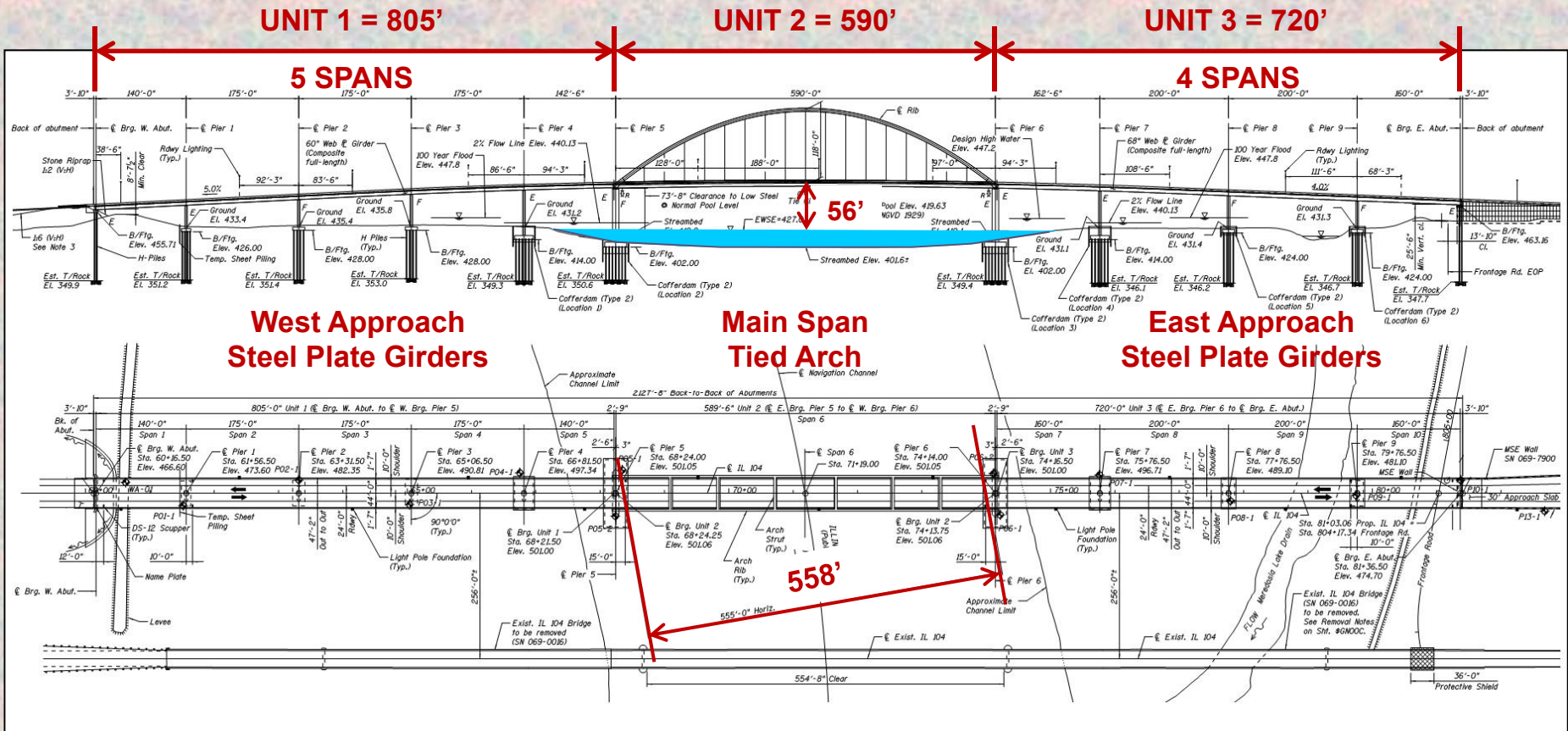


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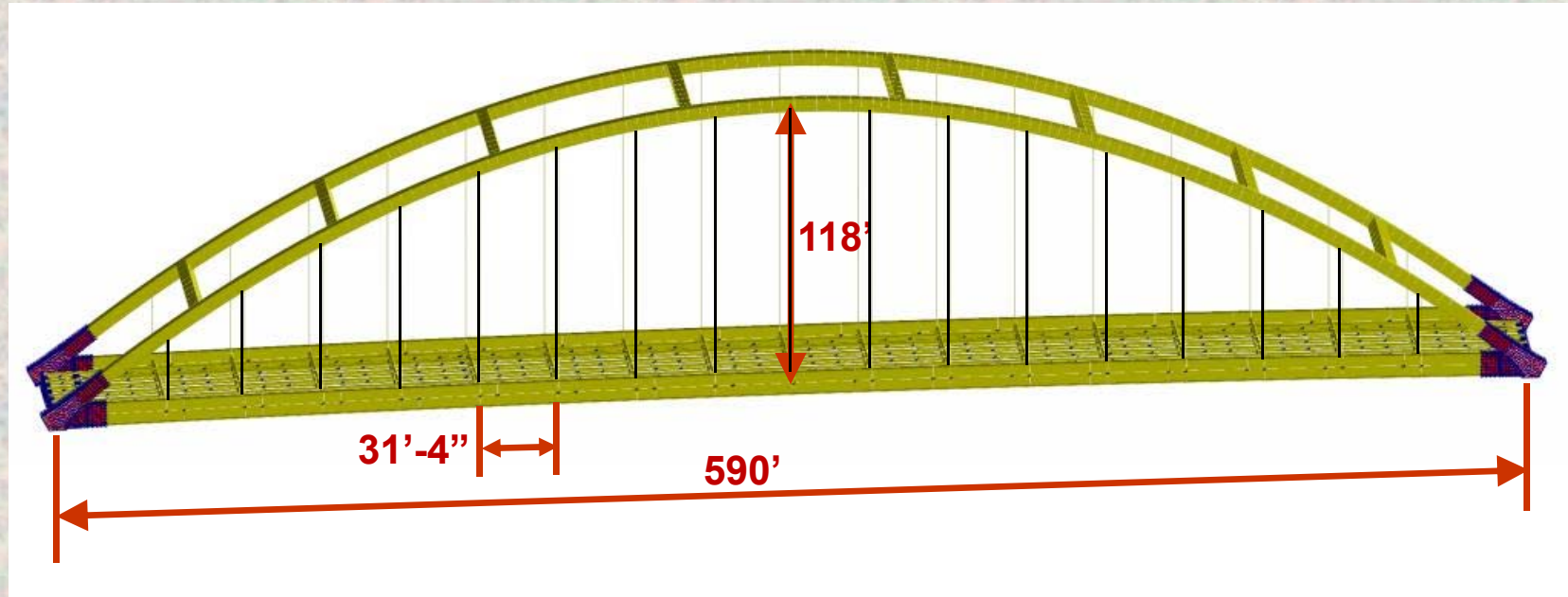
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Proposed River Bridge – General Plan & Elevation

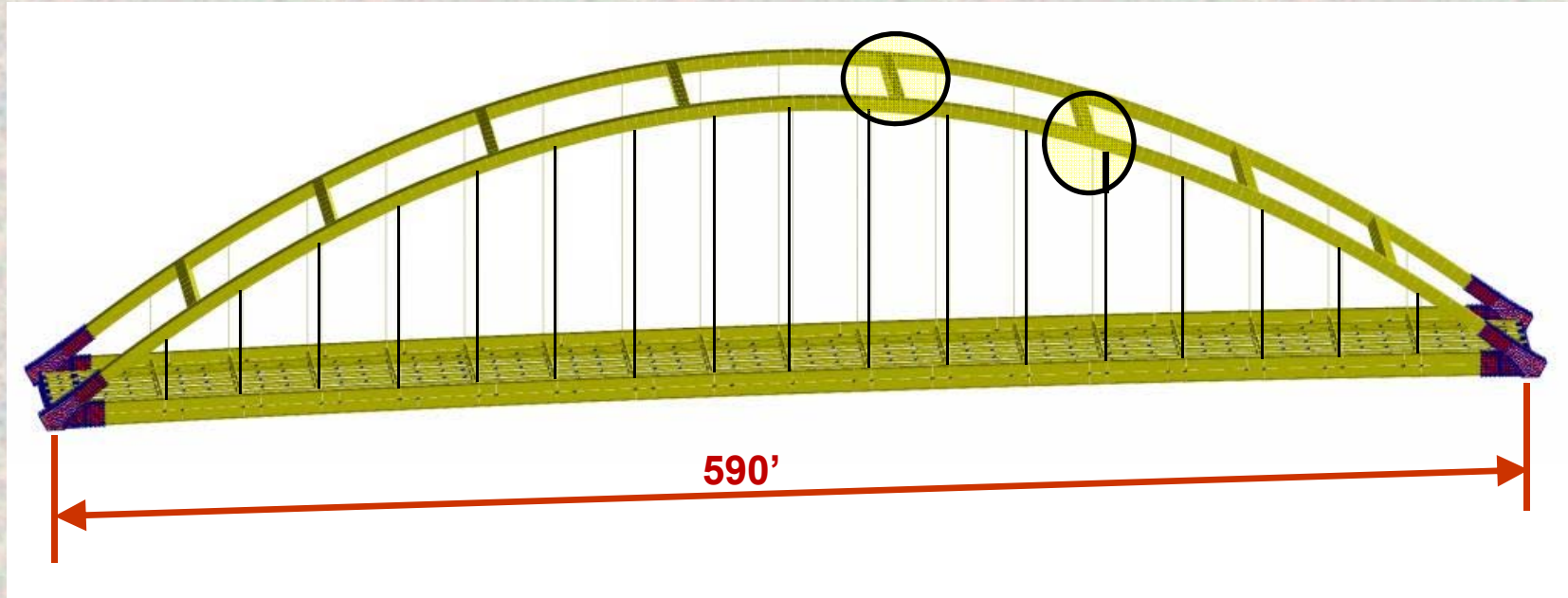


Arch Span Features



- 590-foot span; 118-foot rise (= $1/5^{\text{th}}$ of Span)
- Floor beams & hangers spaced at 31'- 4"

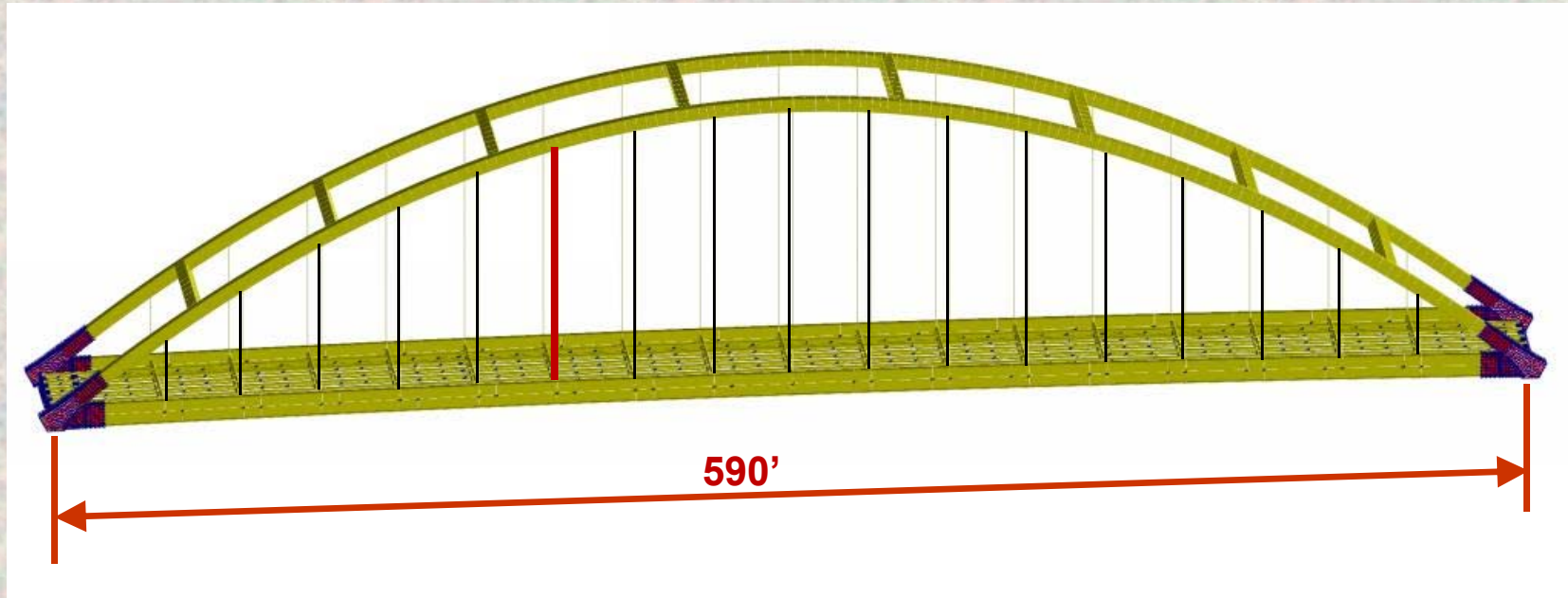
Arch Span Features



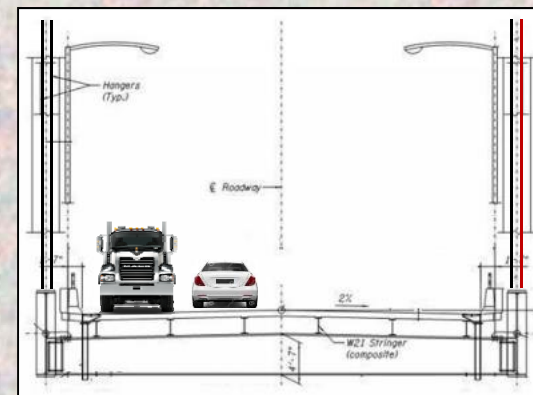
- Rib Bracing – Vierendeel Struts @ approx. 2 times the hanger spacing; No diagonal or “K” bracing; Clean/Open Structure
- Struts are offset from hangers – Simplifies connections of struts and hangers to rib



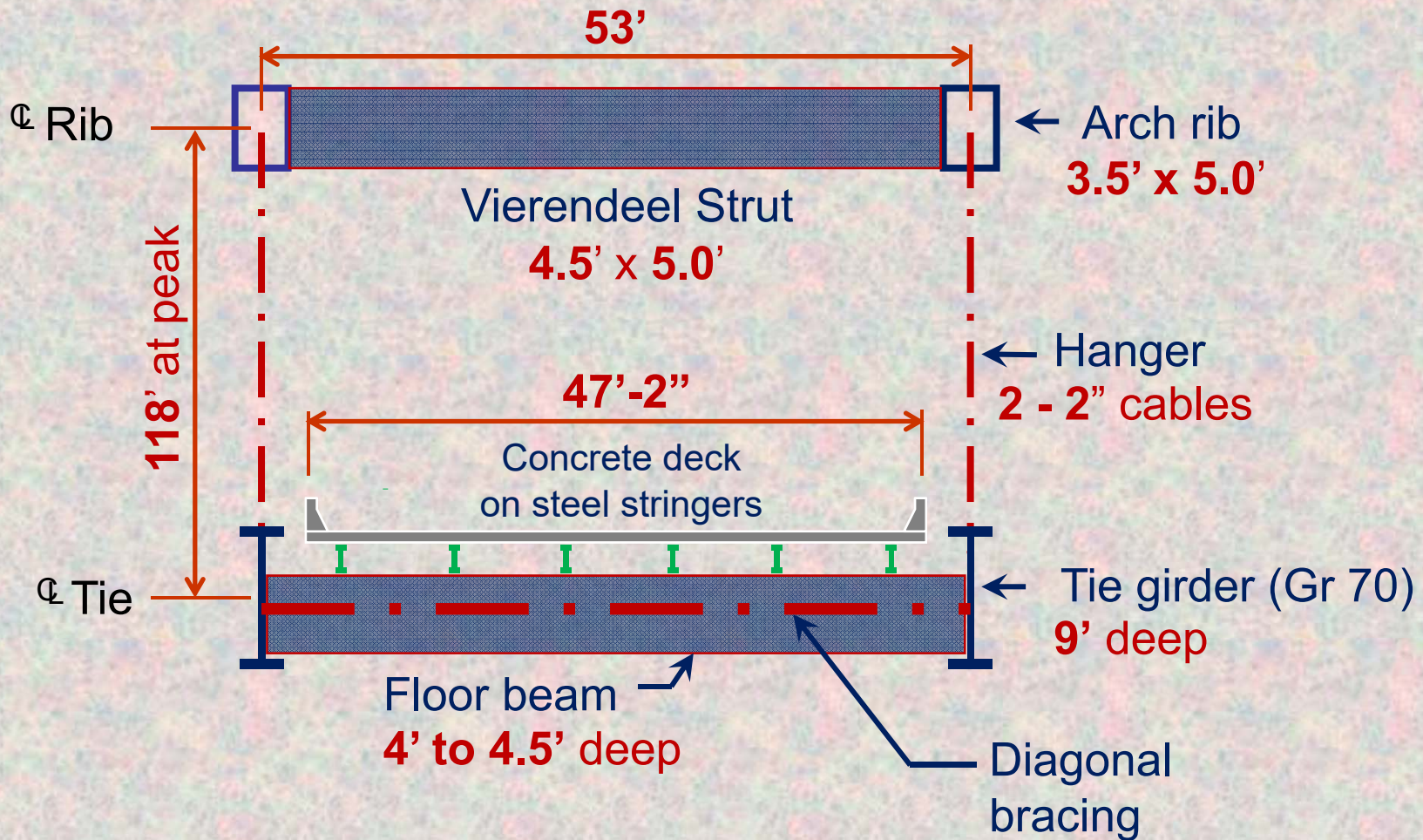
Arch Span Features



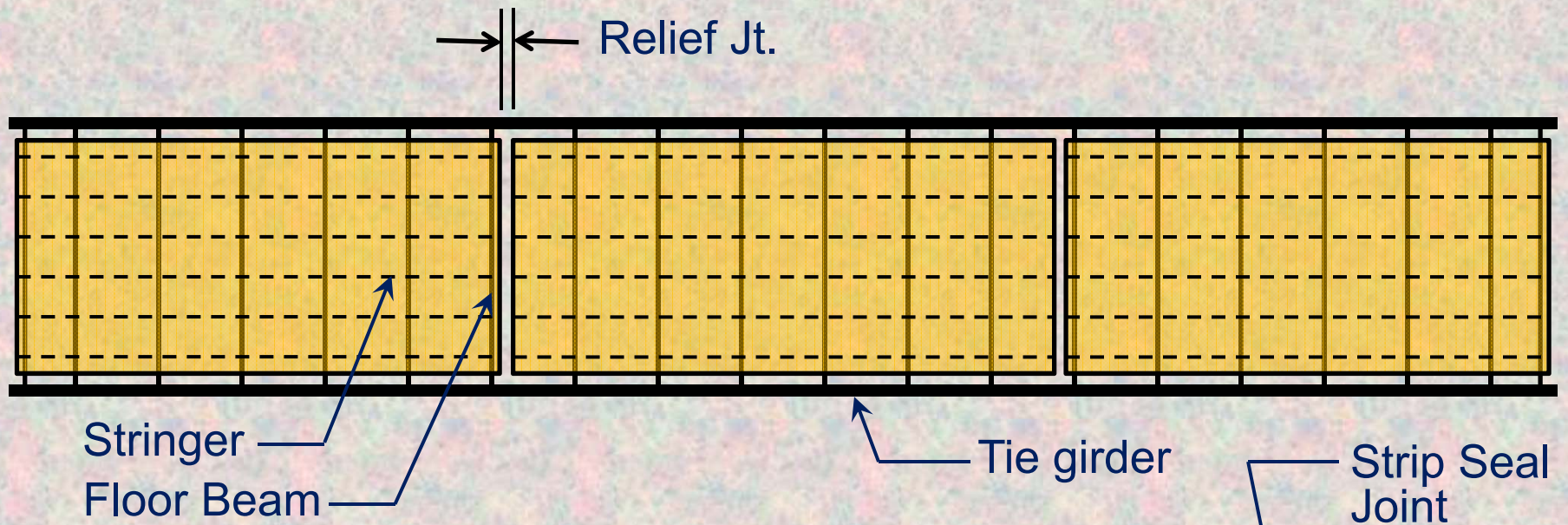
- Redundant hangers (2 – 2" cables)
- With loss of 1 cable or when cable needs to be replaced, a single cable can support two traffic lanes on far side of the deck
- Loss of Complete Hanger – would not collapse nor incur permanent damage



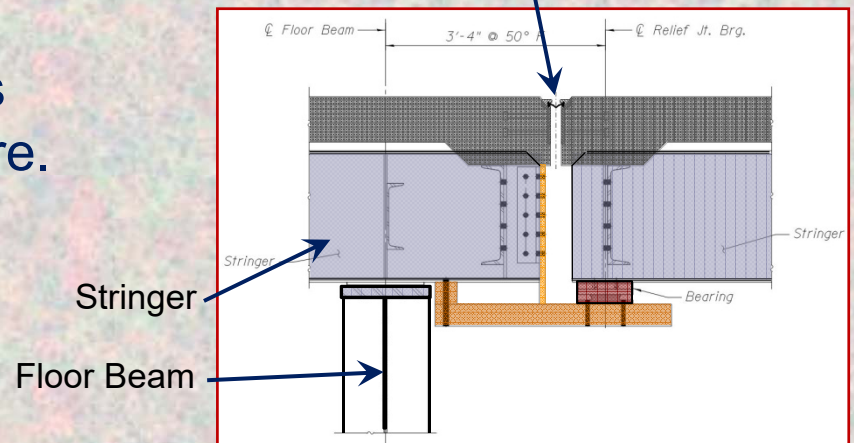
Arch Span Features



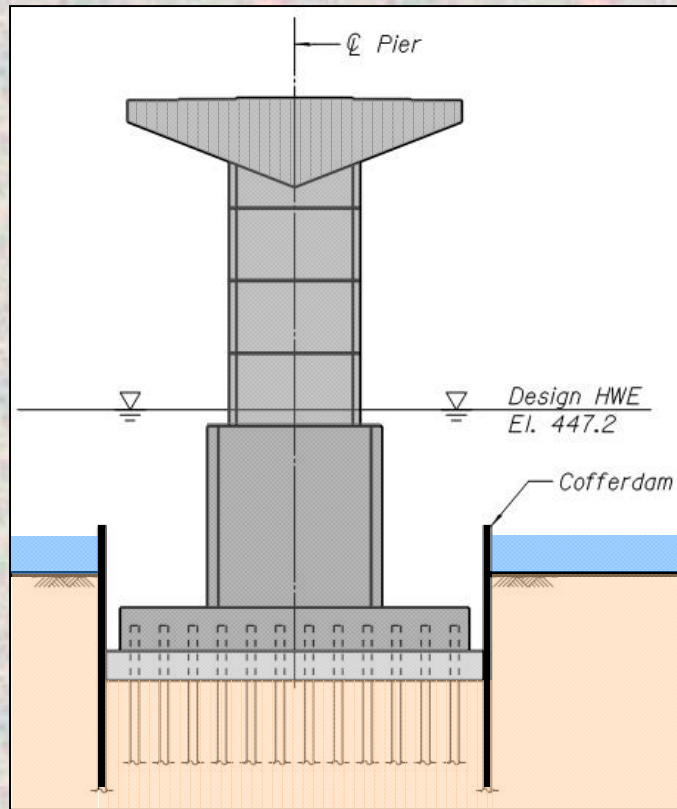
Arch Span Features



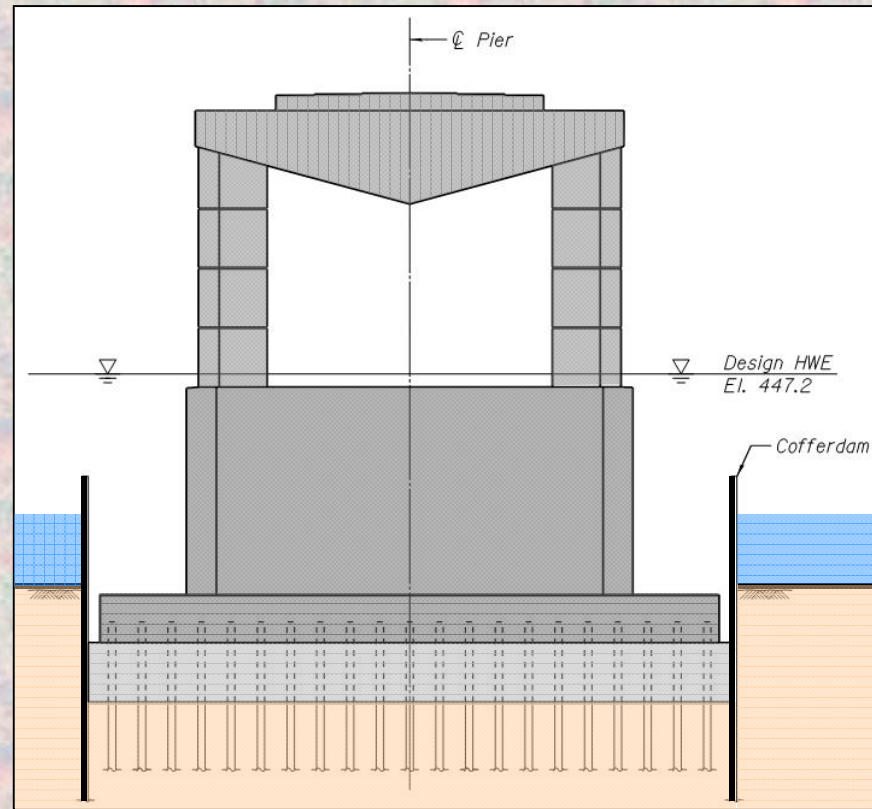
- Relief joints in the deck and stringers uncouple them from the arch structure.
- Allows conventional replacement of the deck and stringers.



Proposed River Bridge – Piers



Approach Piers



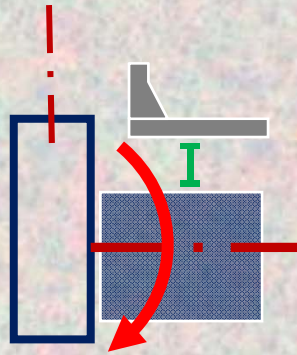
Main Piers

Presentation Outline

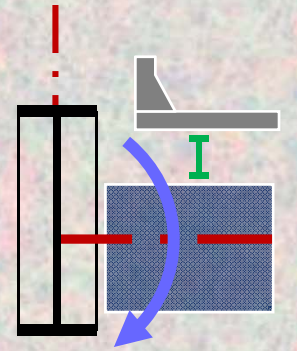
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Tie Girders : I-sections.....not Box-sections



Conventional



This Bridge

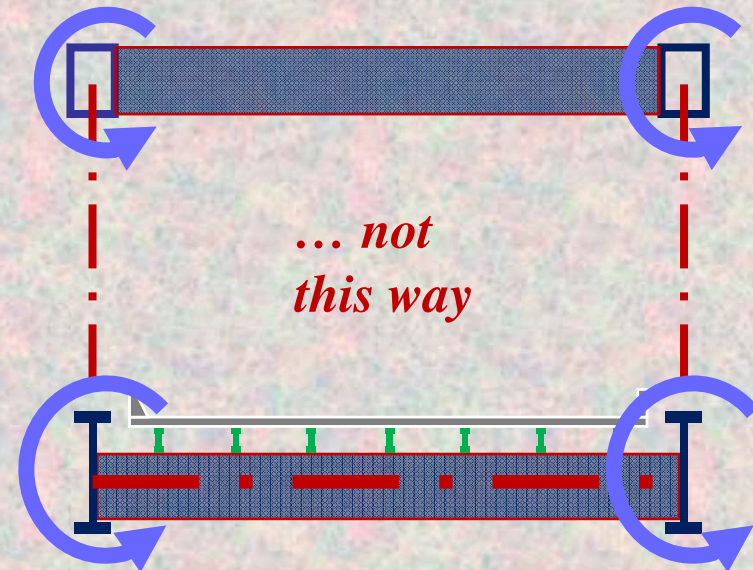
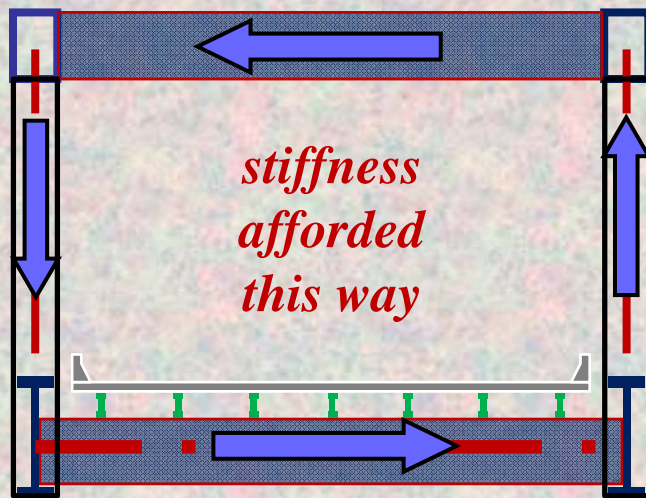
Advantages:

- Very economical
- Greatly simplifies the floor beam connections
- Torsionally flexible; reduces secondary stresses and potential fatigue cracking in FB connections
- Easier to inspect & maintain

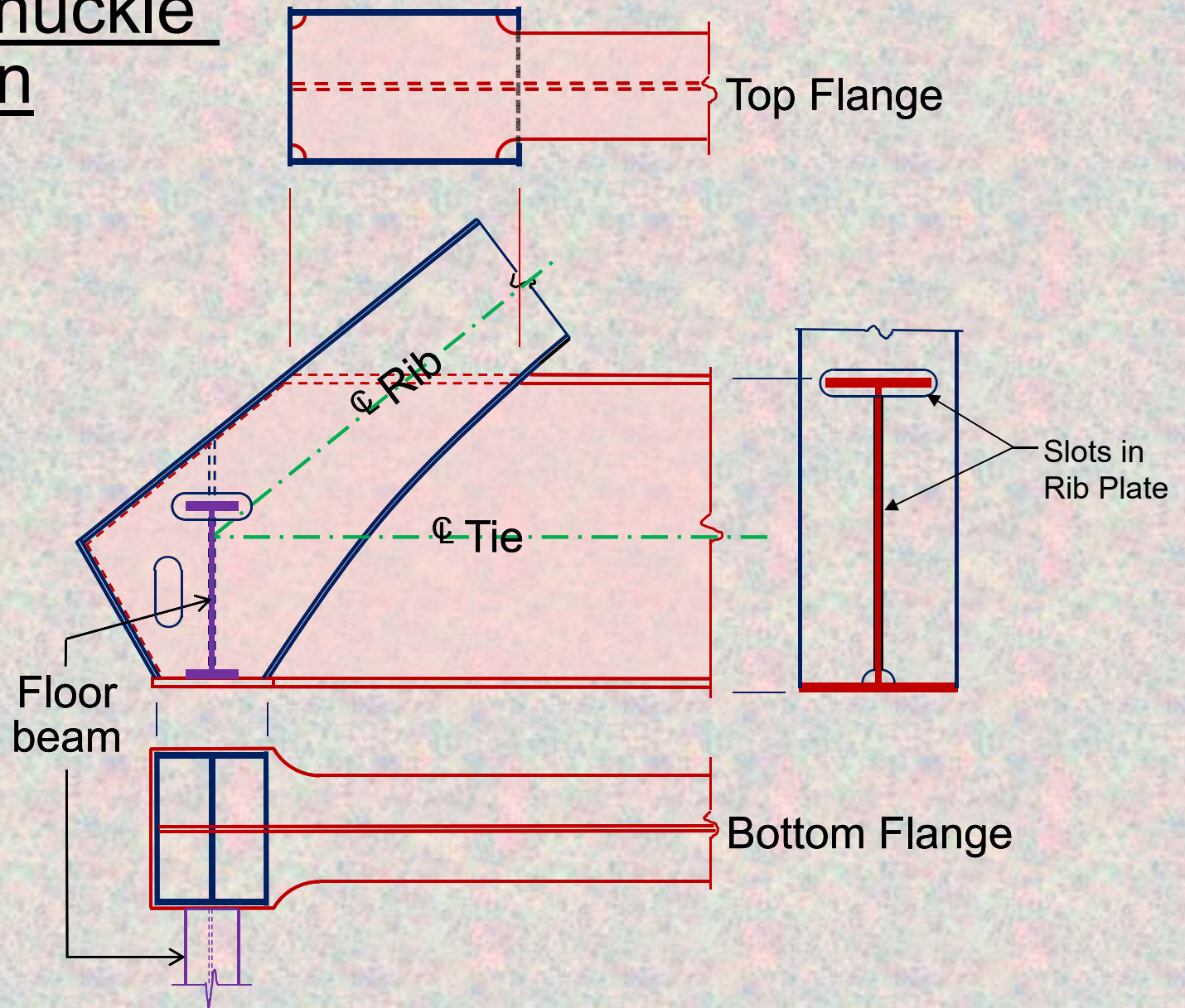
Tie Girders : I-sections.....not Box-sections

Overall Torsional Stiffness:

- No loss of overall torsional stiffness of the arch system



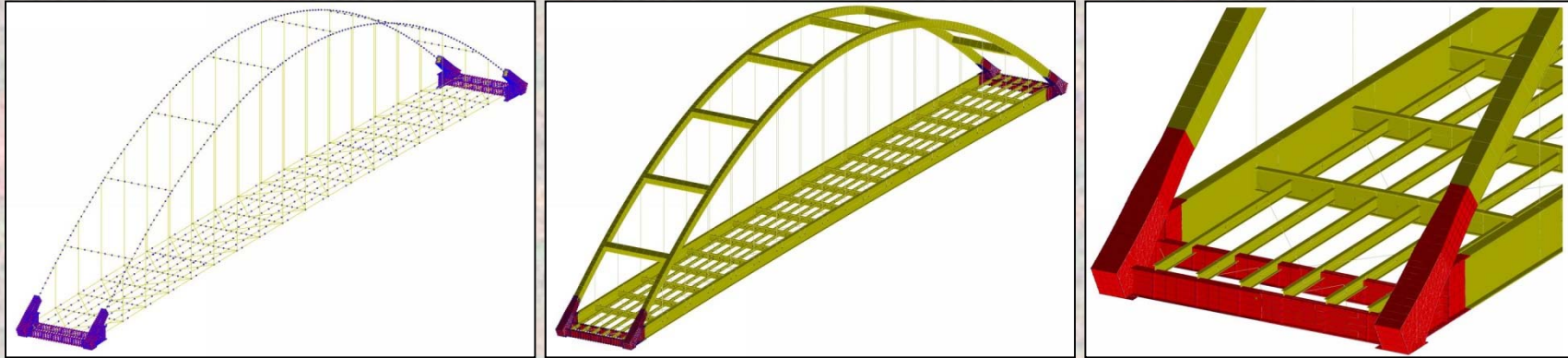
Tie-Rib "Knuckle" Connection



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 - Complex Analysis
 - Unique Design Loads
 - Unique Design Checks
7. Construction

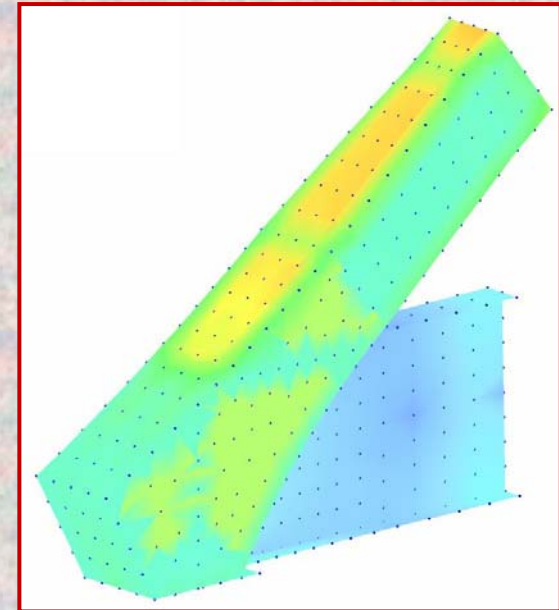
Analysis & Design



- Used LARSA 4D for modeling and analysis
- Modeled as line elements, except plate elements for knuckles and the Floor Beams framing in to the knuckles
- 4,695 nodes

Analysis & Design

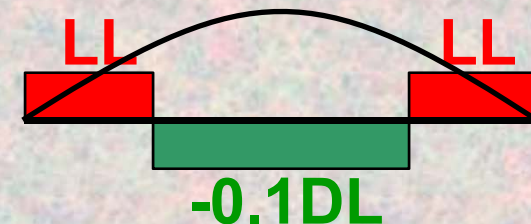
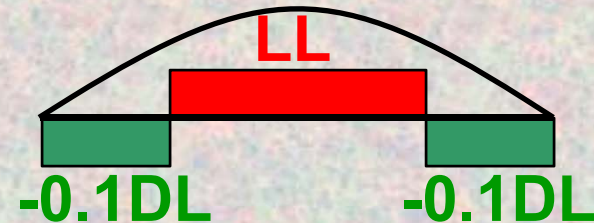
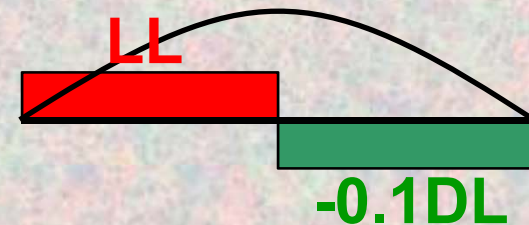
- Live Load – AASHTO HL-93 applied as incrementally moving load
- Variable transverse placements to maximize force effects in various members
- Analysis Data → Force envelopes by member groups
- Strength checks by AASHTO LRFD
- Knuckle behavior not definitive; Stresses checked by stress contours



Unique Design Loads

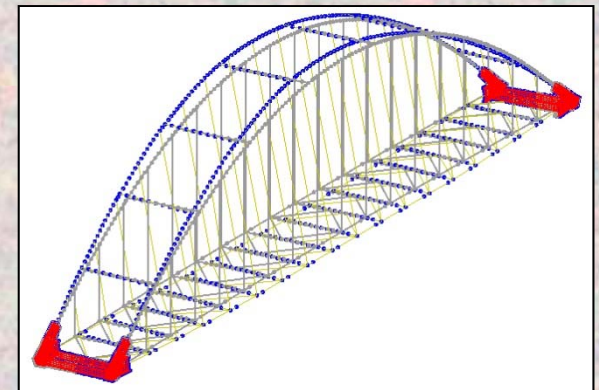
- Nothing in AASHTO on loads specific to arch bridges, which are very sensitive to unbalanced load
- Used these load cases for design:
 - Dead Load
 - Live Load *
 - 10% Dead Load reduction where there is no LL

* Applied as moving loads

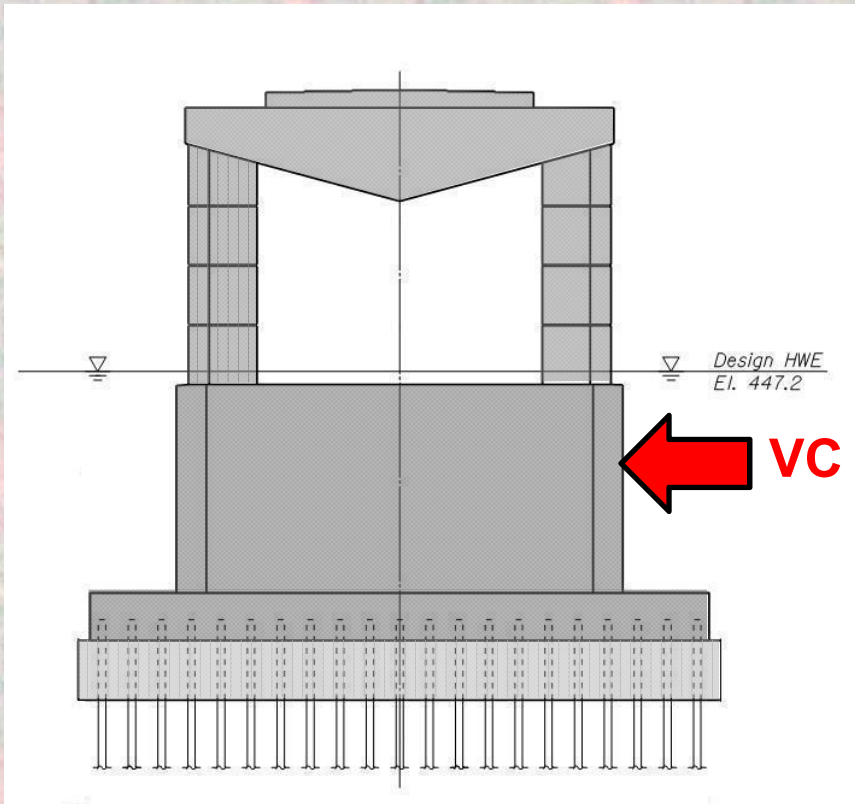


Stability Design of Arch Span

- No guidelines in AASHTO Design Specifications
- Used AISC's **Direct Analysis Method** - commonly used for complex building structures – Most rational & transparent stability design method
- Considered geometric imperfections (L/1000 lateral offset of ribs)
- Considered 20% stiffness reduction to account for unanticipated residual stresses and local yielding
- Performed second-order analysis using LARSA 4D in both vertical and lateral directions
- Strength checks by AASHTO LRFD



Vessel Collision Design

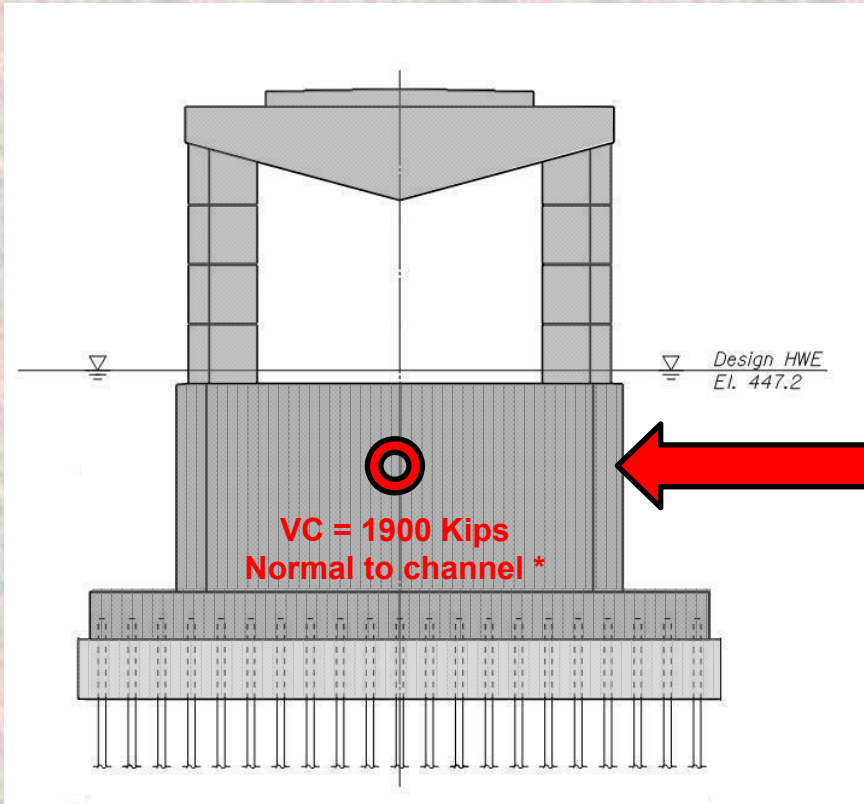


- River traversed by Large / Heavy Barges
- Operational Classification: **Critical Bridge**
- **VC** Force computed using probability based analysis that considered:
 - Waterway depth & geometry – straight or curved
 - Type, size & frequency of Vessels
 - Vessel direction & speed

Vessel Collision Design

Design Vessel

3x5 (15) Barge Tow



**VC = 3800 Kips
Parallel to channel ***

*** Not to be applied
simultaneously**

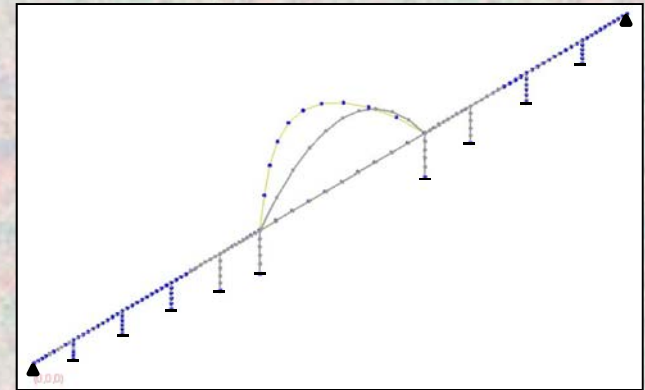
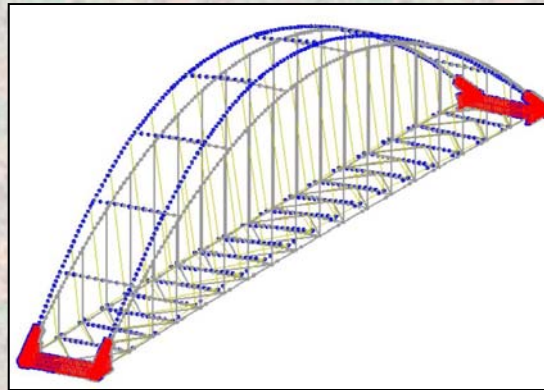
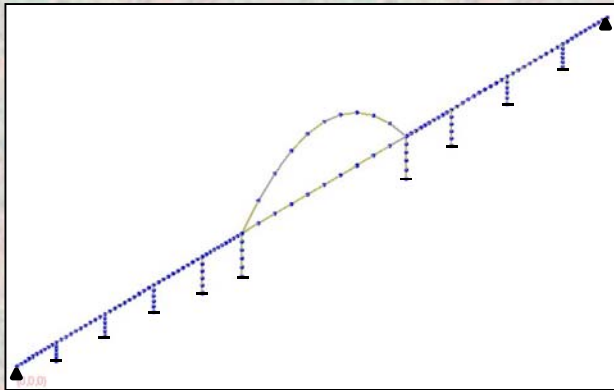
Main Pier

Seismic Analysis & Design

- Bridge location: SPZ “2” and Site Soil Classification “E”
- Seismic Design for 2500-year Return Period
- AASHTO provides Seismic Response Spectrum only for 1000-year return period
- Used 2500-year Response Spectrum provided by NEHRP(*) with a “2/3rd” Design Factor – AASHTO equivalent design for 1500-year return period

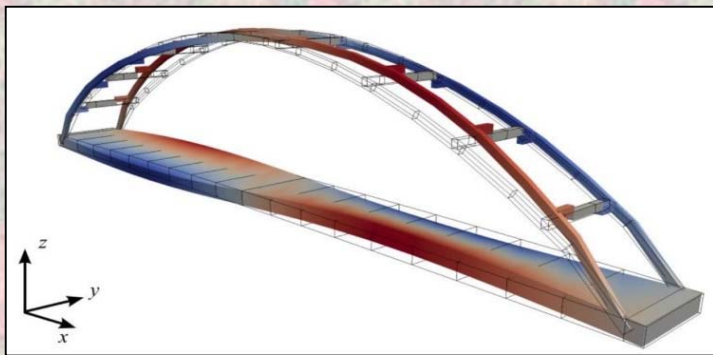
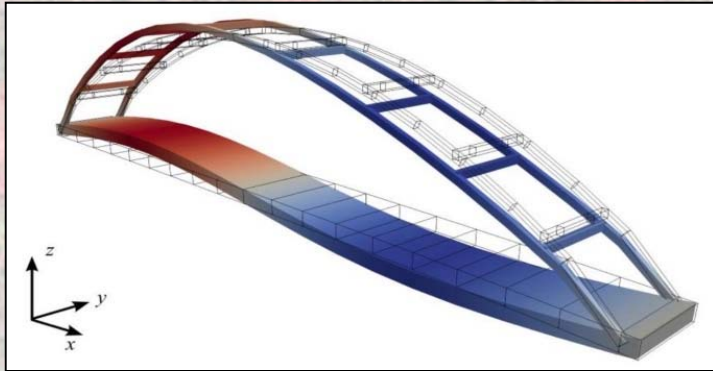
(*) NEHRP = National Earthquake Hazards Reduction Program

Seismic Analysis & Design



- A simplistic 3D linear elastic model of entire bridge –
 - Approach spans as continuous beams
 - Arch as two beams (parabolic – ribs + struts, straight - tie girders + deck); Equivalent mass and stiffness derived by vibration analysis of the full 3D arch model
 - Piers as vertical cantilevers – mass & stiffness of Piers & Foundations
- Elastic model analyzed for various modes & frequencies; Seismic forces were computed by modal superposition using Complete Quadratic Combination (CQC) method.

Aerodynamic Stability – Study by RWDI



1st Stage:

- Analytical Desktop Study – using Computational Fluid Dynamics analysis
- Vibration modes provided by **exp**
- Findings:
 - Provided Wind Loads for Design (*)
 - Aerodynamic Stability Not Clear
 - Testing Required to Confirm Stability

(*) Less than AASHTO loads

Aerodynamic Stability



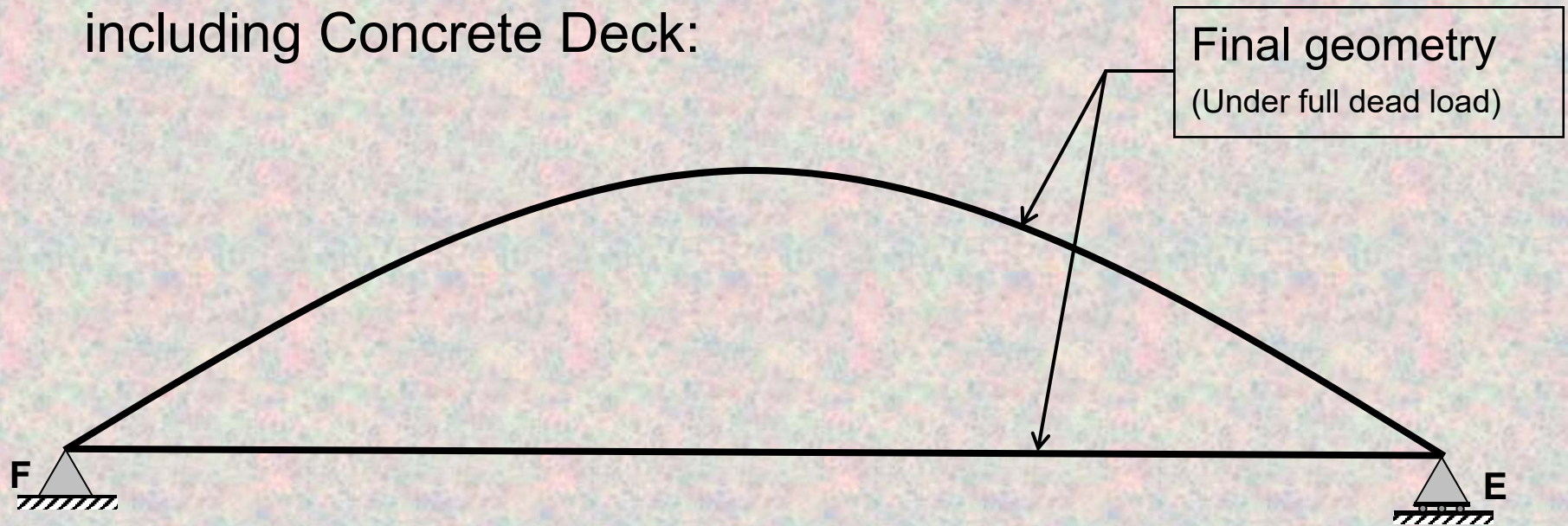
2nd Stage:

- Tested Sectional Model in Wind Tunnel
- Investigated stability against flutter, vortex shedding & galloping
- Findings:
 - Confirmed Aerodynamic Stability
 - Flutter - OK
 - Vortex-Shedding Excitation - OK
 - Galloping - OK



Fabrication Geometry & Pre-stressed Assembly

Fully Constructed Arch Span
including Concrete Deck:

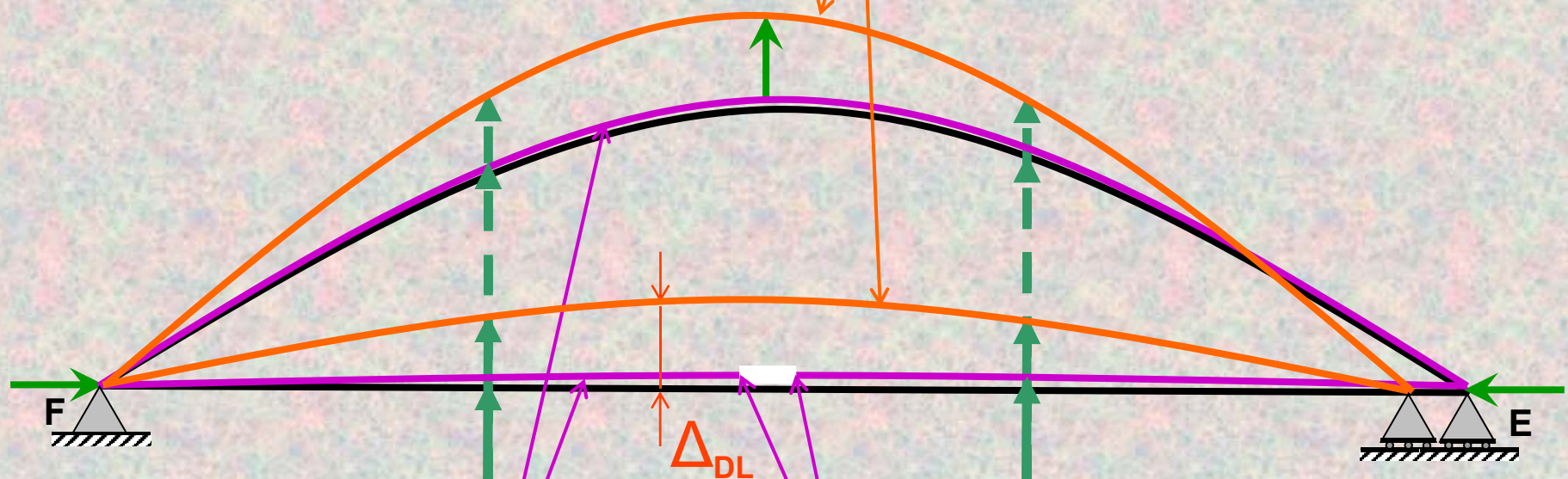


- Conforms to theoretical Roadway Profile after DL displacements
- Has Minimal Flexural Stresses due to Dead Load

Fabrication Geometry & Pre-stressed Assembly

** Require manipulation to fully assemble;
Cambers it up; induces bending stresses
that will counter bending stresses due to
the Dead Loads

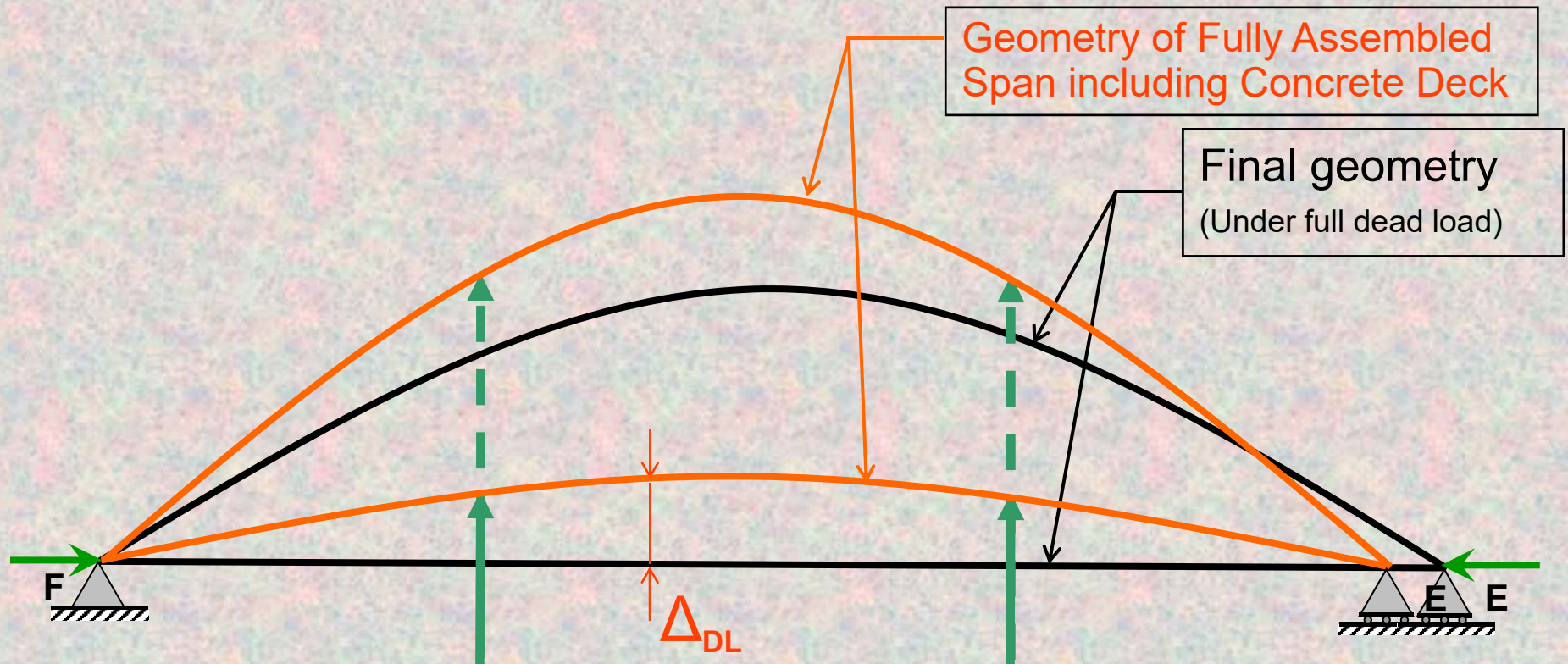
Fully assembled Geometry



Fabricate to
this shape **

Erection on Temporary Shoring;
When assembled in unstressed
condition, the girder ends at
mid-span splice do not meet **

Fabrication Geometry & Pre-stressed Assembly



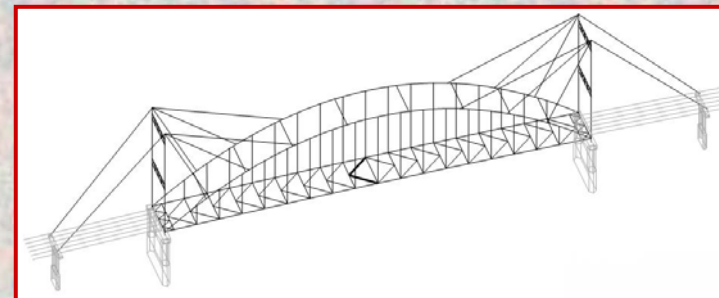
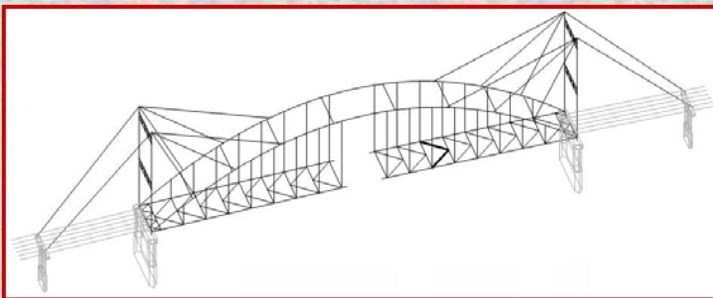
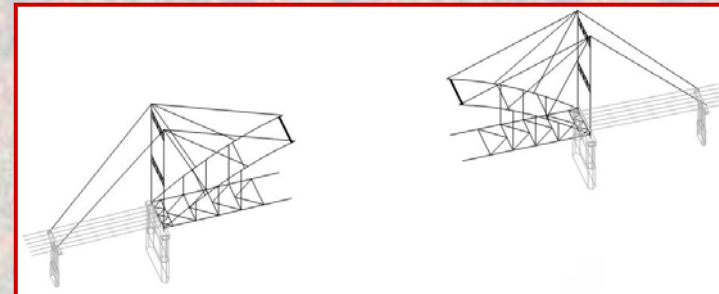
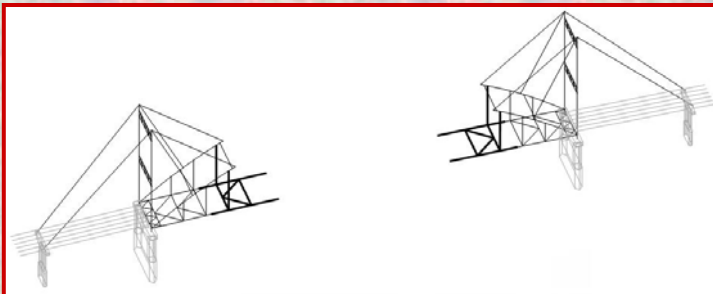
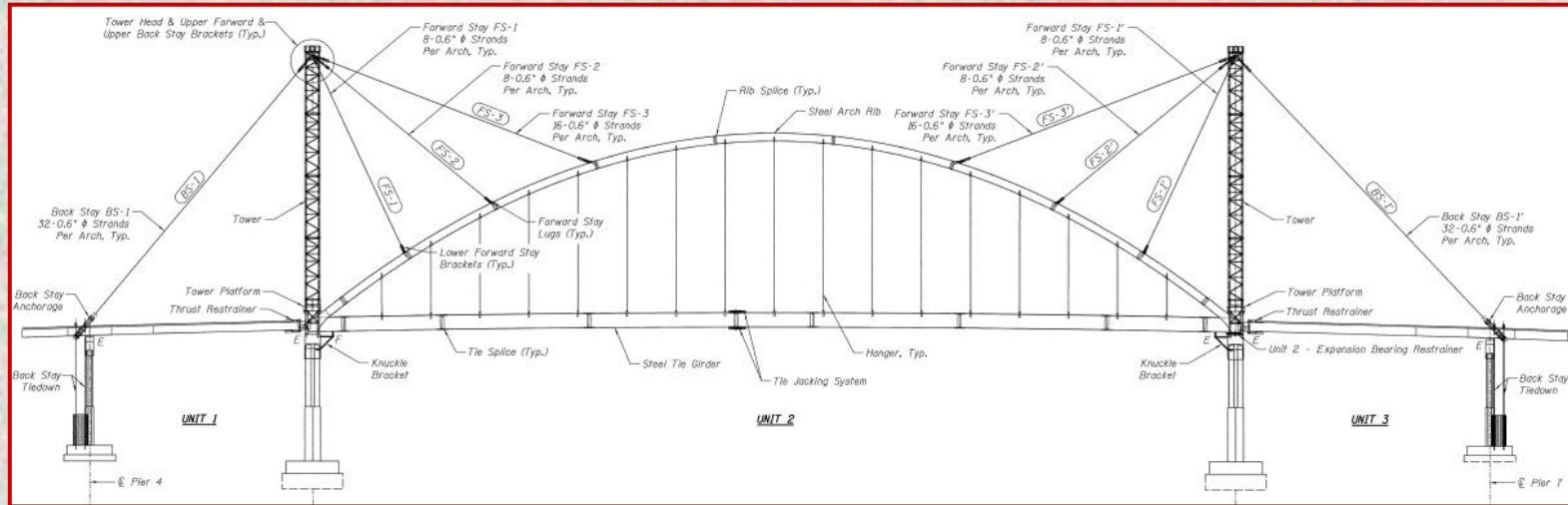
The fabrication geometry was computed working backwards to account for the deflections and bending stresses due to the dead loads

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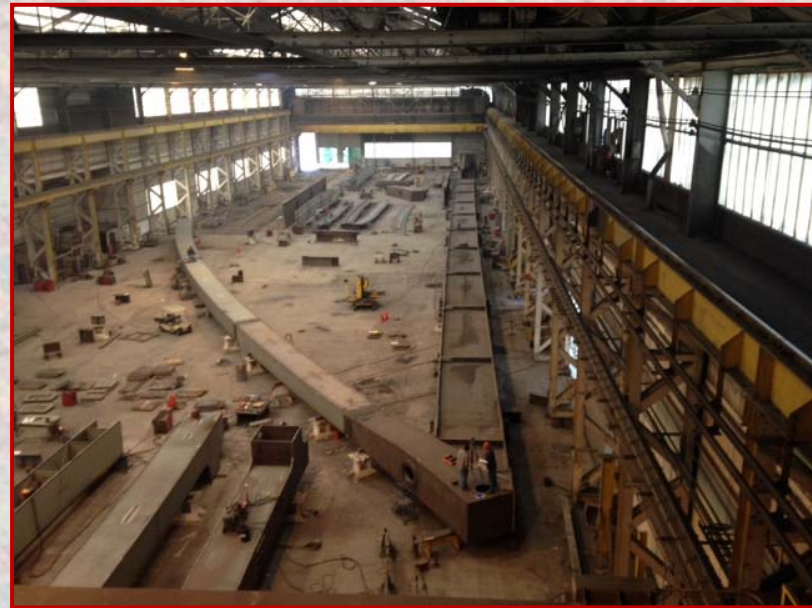
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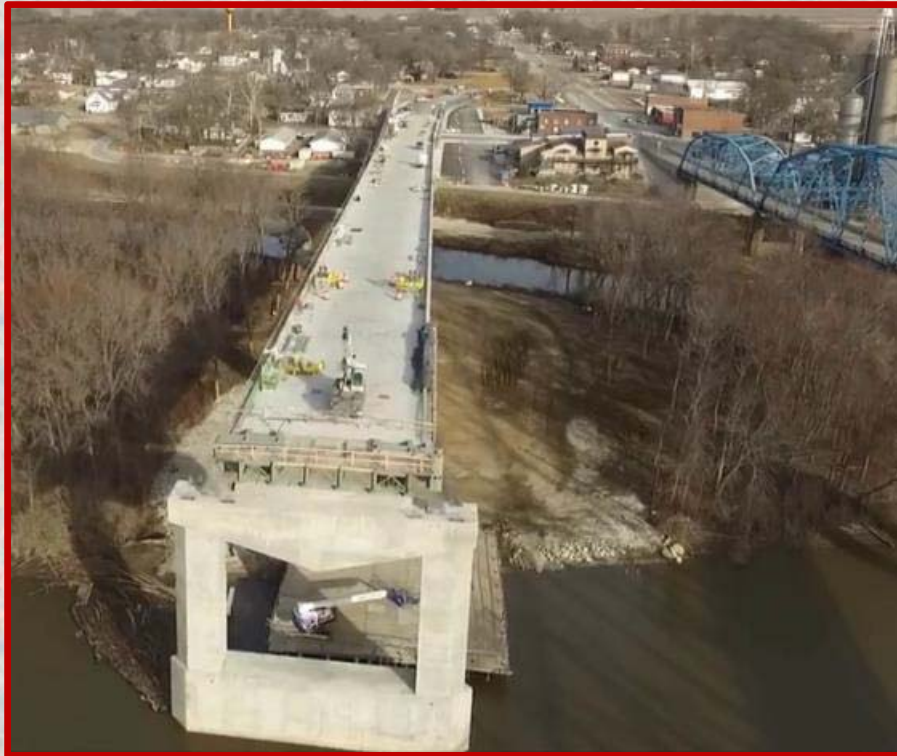
Arch Erection (engineered by Hanson Engineers)



Steel Fabrication / Shop Assembly



Construction – February 2017



East Approach Unit
(looking east)



West Approach Unit
(looking west)

Acknowledgements

Client: Illinois Department of Transportation, District 6
IDOT Bureau of Bridges & Structures
Springfield, IL

Geotechnical: Wang Engineering, Lombard, IL

Peer Review: Alfred Benesch Co., Chicago, IL

Wind Engr'g.: RWDI, Ontario, CN

Contractor: Halverson Construction Co., Springfield, IL

Fabricator: Industrial Steel Construction, Gary, IN

Questions?

